

# Combustion and Error Analysis of Hydrogen and CNG Blends for Multi cylinder SI Engine

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## ABSTRACT

CNG engine emits higher NO<sub>x</sub> as compared to gasoline engine at stoichiometric condition. Lean burn combustion reduces NO<sub>x</sub> emission and gives higher thermal efficiency but increases tendency of misfire and increase cycle by cycle variation. Hydrogen addition extend lean limit, increase thermal eff., combustion speed and reduces combustion duration. This paper shows the effects of hydrogen and CNG blends on Multi-cylinder SI Engine. The combustion and error analysis is done for optimum blend of 5% hydrogen by energy with CNG. All trials are performed at MBT spark timing with WOT conditions. Sequential injection system shows improvement in performance and combustion characteristics of engine.

**Keywords:** HCNG blends, MBT Spark Timing, WOT, COV<sub>pmax</sub> etc.

## 1. Introduction

HCNG is promising alternative fuel. Blends (5, 10, 15, 20 ---- 80%) of H<sub>2</sub> by vol in CNG can be used in single as well as multi-cylinder SI engine. Port Fuel Injection reduces fuel consumption and improves performance and emission characteristics. H<sub>2</sub> addition extend lean operation limit. Hydrogen addition increases thermal efficiency and improves combustion stability. The CP<sub>max</sub>, IMEP and maximum rate of pressure rise increases while burn duration and cycle-by-cycle variation decreases with increase in hydrogen addition at lean operation. Hydrogen addition leads to higher NO<sub>x</sub> if spark timing is not optimized. HC, CO, and CO<sub>2</sub> emission values decreases with increase in hydrogen addition. At lean condition power of HCNG is found to be higher than CNG. Backfiring and pre-ignition are needed to be addressed. In naturally aspirated CNG engine NO<sub>x</sub> emission increases with increase in equivalence ratio NO<sub>x</sub> emission increases with the increase in combustion temperature, duration of high temperature combustion period and the availability of oxygen. HCNG blends with EGR rate has potential to increase brake thermal efficiency of engine with reduction in NO<sub>x</sub> emission compared to CNG engine. Increase in EGR rate slows down combustion with reduction in pumping work and in-cylinder peak temperature.

Hydrogen addition is used to enhance combustion of CNG for improvement in performance and emission of CNG engine. We can also improve the performance and emission characteristic of CNG engine by increasing compression ratio. Higher compression ratio increases brake thermal efficiency due to high octane number of CNG fuel. Dedicated CNG engine of CR=13:1 are more efficient. It is difficult to increase compression ratio of on-road SI engine but can be decreased by removing material from piston surface in case of diesel engines. With slight

modification in cylinder head of existing diesel engine, dedicated CNG engines can be prepared. Injectors are replaced by spark plug and compression ratio is reduced from 22:1 to 13:1. Now days these are run at stoichiometric condition giving higher power output. As CNG has slow flame speed lean burn is not possible as it emits NMHC emissions. The only method to reduce NMHC emissions and improvement in thermal efficiency is to enhance it with high burning velocity fuel i.e. hydrogen. CNG engines give higher in-cylinder pressure only if it is dedicated CNG engine with compression ration 13:1 to 15:1 at stoichiometric condition. The experimentation done on engine is dedicated gasoline stoichio. burn engine with compression ratio 9.2:1. The lower mass density of CNG (0.717) compared to gasoline (5.11) in gaseous form reduces mass intake charge which reduces in-cylinder pressure. Volumetric efficiency of gaseous fuelled engine is less. As CNG is gaseous fuel volumetric efficiency is less and it further decreases with increase in speed which reduces in-cylinder pressure. Liquid Gasoline has higher density than CNG which increases charge intake by mass increasing in-cylinder pressure. Compared to above effect the high octane number and higher calorific value of CNG does not show much improvement in rise in in-cylinder pressure.

## 2. Experimental Setup:



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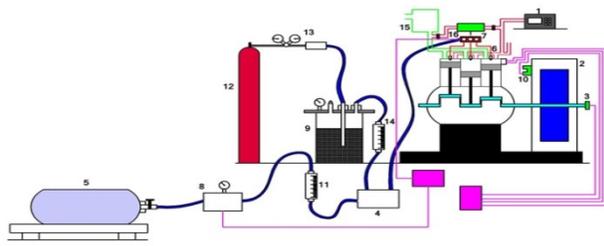


Fig.1 Experimental rig: 1: Exhaust Gas Analyzer, 2: Eddy current Dynamometer, 3: Crank Angle Sensor & rpm sensor, 4: CNG & Hydrogen Mixer, 5: CNG Cylinder, 6: CNG Rail with 3 Injectors, 7: CNG ON/OFF valve, 8: CNG 2 stage regulator, 9: Hydrogen flame trap, 10: Load Cell, 11: CNG Flow meter, 12: hydrogen cylinder, 13: Hydrogen 2 Stage Regulator with Flame Arrestor, 14: Hydrogen Flow-meter and regulator, 15: Air Box with Water Manometer, 16: Oxygen Sensor.

### 3. Results and Discussions

#### Combustion Analysis (MBT, WOT, CR=9.2, $\phi=1.0$ )

Cylinder peak pressure increases with increase in H<sub>2</sub> addition. Hydrogen fast burn speed advance the time of maximum pressure towards TDC.

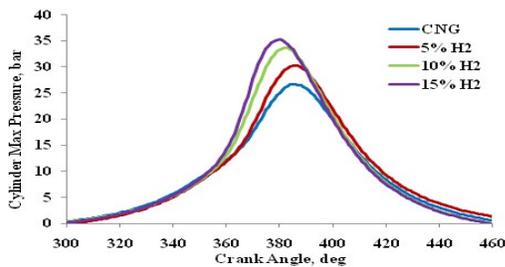


Fig 2: Cpmax of HCNG Blends for Speed

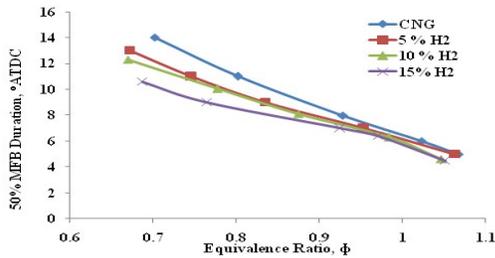


Fig 3: 50% MFB of HCNG Blends for Phi

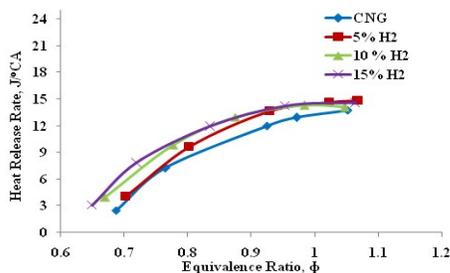


Fig. 4: CPmax of HCNG Blends for Phi

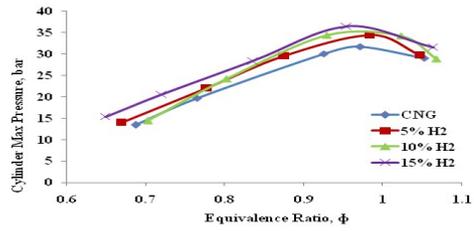


Fig.5: HRR of HCNG blends for Phi

At 3000 rev/min and  $\phi=1.0$ , the maximum peak pressure for 15% hydrogen addition is observed to be 35.17 bar occurred at 19° ATDC. Knocking and pre-ignition never occurred in sequential port fuel injection system (SPFIS) till 15% hydrogen addition. Cylinder pressure decreased with increase in speed. Cylinder peak pressure increases with increase in equivalence ratio. For 5% hydrogen addition and equivalence ratio 0.98 maximum peak pressure of 34.42 bars is observed at 2500 rpm. Combustion duration is the duration in crank angle between 10 to 90% mass fraction burnt at 2500 rpm.

Combustion duration decreases with increase in equivalence ratio and hydrogen addition. For 5% H<sub>2</sub> addition and  $\phi=0.73$ , 50% MFB occurred at 9°ATDC and 4000 rpm. Heat release rate increases with increase in speed and increase in hydrogen addition. HRR is minimum at lean condition.

### 4. Measured Data Repeatability and Accuracy

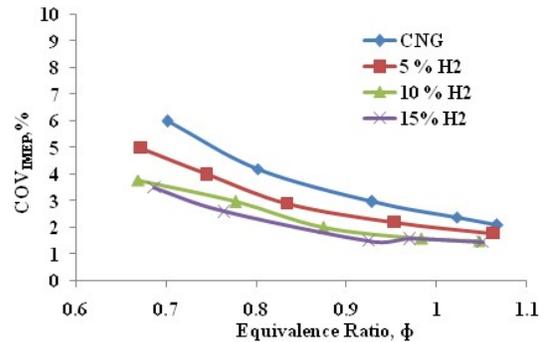


Fig. 6: COVIMEP % of HCNG Blends

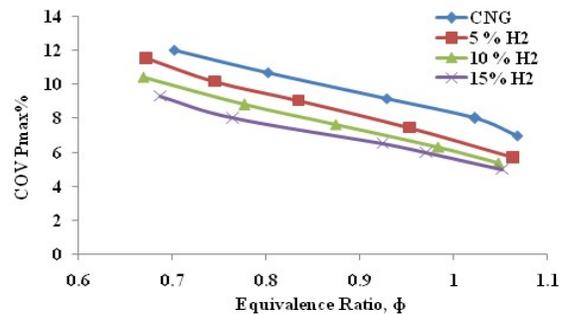
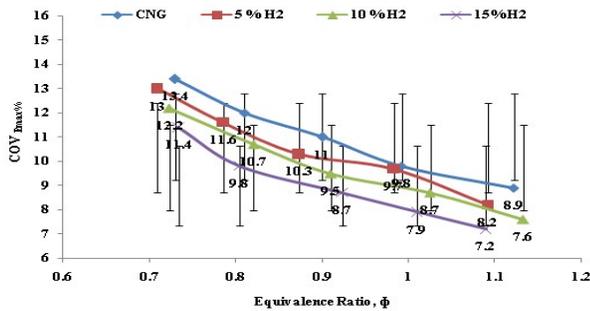


Fig.7: COVPmax% of HCNG Blends

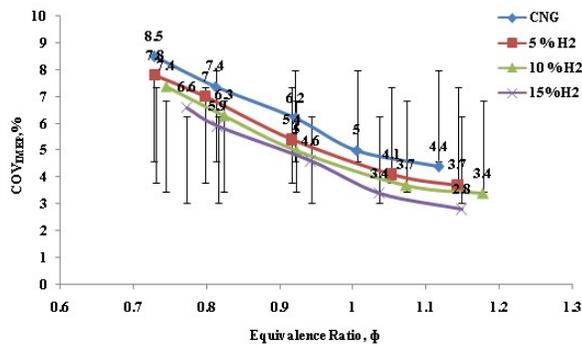
It is the standard deviation of measured magnitude as a percentage of its mean value. COV<sub>IMEP</sub> is minimum at stoichiometric and relatively rich mixture and suddenly increases as the lean limit is approached. The

COV<sub>IMEP</sub> and COV<sub>Pmax</sub> are calculated from the P- $\phi$  diagram for 10 average cycles. The decrease in COV<sub>IMEP</sub> of HCNG blends shows engine lean burn stability is greatly improved by hydrogen addition. COV<sub>IMEP</sub> is less than 10 % for equivalence ratio of 0.6. COV<sub>Pmax</sub> is better in HCNG blends compared to CNG. COV<sub>IMEP</sub> decreased with increase in speed and increase in hydrogen addition and maintained low level at  $\phi=1.0$ . The decrease in COV<sub>IMEP</sub> and COV<sub>Pmax</sub> shows engine stability is greatly improved by hydrogen addition. At higher speed & WOT condition and equivalence ratio 1.0 due to rich fuel air mixture the combustion temperature increases which increases detonation. This gives rise to COV<sub>Pmax</sub> at higher speed. Minimum COV<sub>Pmax</sub> of 6% is observed at 2500 rpm for gasoline & CNG. Higher COV<sub>Pmax</sub> is observed for gasoline than CNG due to higher charge by mass. COV<sub>Pmax</sub> for gasoline is observed 12.8% and CNG 11.27% at 4000 rpm.

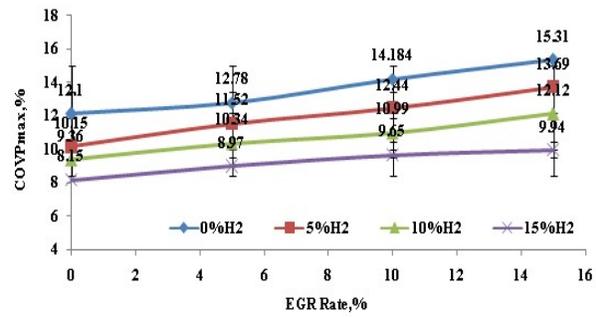
**5. Error bar for COV<sub>Pmax</sub> is done by doing uncertainty analysis:**



**Fig. 8: Coefficient of Variance of Pmax as a function of Equivalence Ratio at a constant speed of 4000 rpm for different fuel blends**



**Fig. 9: Coefficient of Variance of IMEP as a function of Equivalence Ratio at a constant speed of 4000 rpm for different fuel blends**



**Fig 10: Coefficient of Variance of Pmax as a function of EGR rate at 3500 rpm and equivalence ratio 1.0**

**Table 1. CNG**

CNG						
Equivalence Ratio	Dev Pmax	COV Pmax	Dev IMEP	COV IMEP	Dev RPR	COV RPR
0.727033	1.44	0.31	0.1	23	0.01	2.75
0.822405	0.7	4.4	1.43	21.7	0.0097	2.64
0.909091	2.63	11.55	0.4	5.48	0.084	14.81
1	3.32	12.02	0.399	5.06	0.186	22.73
1.190595	3.54	10.28	0.325	3.47	0.307	21.04

**6. Conclusion**

From the present investigation it is found that sequential injection system proved to be more efficient for HCNG operation for reduction in backfire and increase in brake thermal efficiency. 5% hydrogen addition by energy is observed to be optimum blend for improvement in performance and reduction in emission. Lean burn combustion is easily achieved with hydrogen addition for improvement in brake thermal efficiency. Existing on-road S.I engines can be easily converted to HCNG sequential port fuel injection system (SPFIS) with slight modification.

**REFERENCES**

- [1] Erjiang Hu, Zuohua Huang, Bing Liu. Experimental study on combustion characteristics of a spark ignition engine fuelled with natural gas hydrogen blends combining with EGR. International Journal of Hydrogen Energy 2009; 34: 1035-1044.
- [2] Bilge Albrayrak Ceper et al. Investigation of cylinder pressure for H<sub>2</sub>/CH<sub>4</sub> mixtures at different loads. International Journal of Hydrogen Energy 2009; 34:4855-4861.
- [3] Thipse S. S., Rairikar S. D. Development of a six cylinder HCNG engine using an optimized lean burn concept. SAE International 2009-26-031.
- [4] Khatri D. S. HCNG evaluation using a sequential gas injection system for a passenger car. SAE International 2009-26-30.

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- [5] Unich A, Morrone B. The impact of natural gas-hydrogen blends on internal combustion engines performance and emissions. SAE International 2009-24-0102.
- [6] Erjiang Hu, Zuohua Huang, Bing Liu. Experimental investigation on performance and emissions of a spark ignition engine fuelled with natural gas hydrogen blends combined with EGR. International Journal of Hydrogen Energy 2009; 34: 528-539.
- [7] Thurnheer T, Soltic P. An SI engine fuelled with gasoline, methane and methane/ hydrogen blends: Heat release and loss analysis. International Journal of Hydrogen Energy 2009; 34: 2494-2503.
- [8] Yujun Wang, Xin Zhang. Experimental and modeling study of performance and emissions of SI engine fuelled by natural gas hydrogen mixtures. International Journal of Hydrogen Energy 2009; 32: 1-4.
- [9] Jinhua Wang, Zuohua Huang. Numerical study of the effect of hydrogen addition on methane-air mixture combustion. International Journal of Hydrogen Energy 2009; 34: 1084-1096.
- [10] Thipse S. S. Development of HCNG blended fuel engine with control of NOx emissions. International Journal of Computer Information Systems and Industrial Management Applications 2010; 02: 087-095.
- [11] Escalante Soberanis M. A, Fernandez A. M. A review on the technical adaptations for internal combustion engines to operate with gas/hydrogen mixtures. International Journal of Hydrogen Energy 2010; 35: 12134-12140.